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## Standard ECMA-396

# Test Method for the Estimation of Lifetime of Optical Media for Long-term Data Storage 



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## Introduction

Markets and industry have developed a common understanding that the property referred to as the lifetime of data recorded to optical media plays an increasingly important role for the intended applications. Disparate standardized test methodologies exist for Magneto Optical media and recordable compact disk and DVD systems. It was agreed that the project represented by this document be undertaken in order to provide a common methodology, applicable for various purposes, that includes the testing of currently available writable CD and DVD optical media.

ISO/IEC JTC 1/SC 23/JWG 1, which is a Joint working group among ISO/TC 42, ISO/TC 171 and ISO/IEC JTC 1/SC 23, initiated work on this subject and developed the initial drafts with assistance from Ecma International TC31.

This Ecma Standard has been adopted by the General Assembly of December 2010.
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## Test Method for the Estimation of Lifetime of Optical Media for Long-term Data Storage

## 1 Scope

This Ecma Standard specifies an accelerated aging test method for estimating the lifetime of the retrievability of information stored on recordable or rewritable optical disks.

This test includes details on the following formats: DVD-R/RW/RAM, $+R /+R W$ and $C D-R / R W$. It may be applied to additional optical disk formats, with substitution of the appropriate specifications, and may also be updated by committee in the future as required.

This document includes:

- stress conditions

Basic stress condition and Rigorous stress condition testing for use with the Eyring Method and testing for use with the Arrhenius Method

- ambient storage conditions in which the lifetime of data stored on optical media is estimated
- Controlled storage condition, e.g. $25{ }^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$, representing well-controlled storage conditions with full-time air conditioning. Eyring Method is used to estimate the lifetime under this storage condition.
- Harsh storage condition, e.g. $30^{\circ} \mathrm{C}$ and $80 \% \mathrm{RH}$, representing the most severe conditions in which users handle and store the optical media. Arrhenius Method is used to estimate the lifetime under this storage condition.
- evaluation system description
- specimen preparation and data-acquisition procedure
- definition of and method for estimating lifetime of stored data on specified media
- data analysis for lifetime of stored data
- reporting format for estimated lifetime of stored data

The methodology includes only the effects of temperature ( $T$ ) and relative humidity ( RH ). It does not attempt to model degradation due to complex failure-mechanism kinetics, nor does it test for exposure to light, corrosive gases, contaminants, handling, or variations in playback subsystems. Disks exposed to these additional sources of stress or higher levels of temperature and relative humidity are expected to experience shorter usable lifetimes.

## 2 Conformance

Media tested by this methodology shall conform to all normative references specific to that media format.

## 3 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ECMA-130 Data Interchange on Read-only 120 mm Optical Data Disks (CD-ROM) (ISO/IEC 10149:1995)
ECMA-267 120 mm DVD - Read-Only Disk, 3rd edition (ISO/IEC 16448:2002)
ECMA-268 80 mm DVD - Read-Only Disk, 3rd edition (ISO/IEC 16449:2002)
ECMA-330 120 mm (4,7 Gbytes per side) and 80 mm (1,46 Gbytes per side) DVD Rewritable Disk (DVDRAM), 3rd edition (ISO/IEC 17592:2004)

ECMA-337 120 mm and 80 mm - Optical Disk using +RW Format - Capacity: 4,7 and 1,46 Gbytes per side (Recording speed up to 4X), 4th edition (ISO/IEC 17341:2009)

ECMA-338 80 mm (1,46 Gbytes per side) and 120 mm (4,70 Gbytes per side) DVD Re-recordable Disk (DVD-RW) (ISO/IEC 17342:2004)

ECMA-349 120 mm and 80 mm Optical Disk using +R Format - Capacity: 4,7 and 1,46 Gbytes per Side (Recording speed up to 16X), 4th edition (ISO/IEC 17344:2009)

ECMA-359 80 mm (1,46 Gbytes per side) and 120 mm (4,70 Gbytes per side) DVD Recordable Disk (DVDR) (ISO/IEC 23912:2005)

ECMA-364 120 mm and 80 mm Optical Disk using +R DL Format - Capacity: 8,55 and 2,66 Gbytes per Side (Recording speed up to $8 x$ ), 3rd edition (ISO/IEC 25434:2008)

ECMA-371 120 mm and 80 mm Optical Disk using +RW HS Format - Capacity: 4,7 and 1,46 Gbytes per Side (Recording speed 8X) 2nd edition (ISO/IEC 26925:2009)

ECMA-374 120 mm and 80 mm Optical Disk using +RW DL Format - Capacity: 8,55 and 2,66 Gbytes per Side (Recording speed 2,4x) 2nd edition (ISO/IEC 29642:2009)

ECMA-382 120 mm (8,54 Gbytes per side) and 80 mm (2,66 Gbytes per side) DVD Recordable Disk for Dual Layer (DVD-R for DL) (ISO/IEC 12862:2009)

ECMA-384 120 mm (8,54 Gbytes per side) and 80 mm (2,66 Gbytes per side) DVD re-recordable disk for dual layer (DVD-RW for DL) (ISO/IEC 13170: 2009)

ECMA-394 Recordable Compact Disc Systems CD-R Multi-Speed
ECMA-395 Recordable Compact Disc Systems CD-RW Ultra-Speed

## 4 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

## 4.1 <br> Arrhenius method

accelerated aging model based on the effects of temperature only

## 4.2

## baseline

initial test analysis measurements (e.g., initial data errors) after recording and before exposure to a stress condition, i.e. measurement at stress time $t=0$ hours

## 4.3

## basic stress conditions

accelerated aging conditions for estimating the lifetime of data stored on optical media in a reasonable amount of time and labour

## 4.4

$B_{5}$ Life
5 percentile of the lifetime distribution (i.e. $5 \%$ failure time) or $95 \%$ survival lifetime

## 4.5

( $B_{5}$ Life) ${ }_{\text {L }}$
95 \% lower confidence bound of $B_{5}$ life

## 4.6

$B_{50}$ Life
50 percentile of the lifetime distribution (i.e. $50 \%$ failure time) or $50 \%$ survival lifetime

## 4.7 <br> controlled storage condition

well-controlled storage conditions with full-time air conditioning ( $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ ) in which the lifetime of data stored on optical media may be extended

## 4.8

Eyring method
accelerated aging model based on the effects of temperature and relative humidity

## 4.9 <br> data error

data error on the sample disk measured before error correction is applied

### 4.10

## harsh storage condition

most severe conditions in which users handle and store the optical media ( $30^{\circ} \mathrm{C}$ and $80 \% \mathrm{RH}$ ) in which the lifetime of data stored on optical media may be shortened

### 4.11

incubation
process of enclosing and maintaining controlled test-sample environments

### 4.12 <br> maximum data error

maximum data error measured anywhere in one of the relevant areas on the disk:

- for DVD-R/RW and $+\mathrm{R} /+\mathrm{RW}$, this is the Maximum PI Sum 8,
- for DVD-RAM, this is the Maximum BER, and
- for CD-R/RW, this is the Maximum C1 Ave 10.


### 4.13 <br> retrievability <br> ability to recover physically-recorded information as recorded

### 4.14 <br> rigorous stress conditions

accelerated aging conditions for estimating the lifetime of data stored on optical media with higher confidence

### 4.15

stress
temperature and relative humidity variables to which the sample is exposed for the duration of test incubation intervals

### 4.16

## system

combination of hardware, software, storage medium and documentation used to record, retrieve and reproduce information

## 5 Conventions and notations

### 5.1 Representation of numbers

A measured value is rounded off to the least significant digit of the corresponding specified value. For instance, it follows that a specified value of 1,26 with a positive tolerance of $+0,01$ and a negative tolerance of $-0,02$ allows a range of measured values from 1,235 to 1,275.

### 5.2 Names

The names of entities, e.g. specific tracks, fields, zones, etc. are capitalized.

## 6 List of acronyms

BER byte error rate
BLER block error rate

PI parity (of the) inner (code)

## Section 2 - Test and Evaluation

## 7 Measurements

### 7.1 Summary

### 7.1.1 Stress Incubation and Measuring

A sampling of disks will be measured at four stress conditions for the Basic stress condition testing or five stress conditions for the Rigorous stress condition testing for use with the Eyring Method, or three stress condition for the Basic stress condition testing or four stress conditions for the Rigorous stress condition testing for use with the Arrhenius Method.

Each stress condition's total time will be divided into sub-interval time periods. Each disk in each group of disks will have its initial data errors measured before their exposure to stress conditions. Thereafter, each disk will be measured for its data errors after each stress condition incubation sub-interval time period.

The control disk for monitoring of tester can also be measured following each incubation time interval.

### 7.1.2 Assumptions

This Standard makes the following assumptions for applicability of media to be tested specimen life distribution is appropriately modelled by a statistical distribution,
the Eyring Method can be used to model acceleration with the both stresses involved (temperature and relative humidity),
the dominant failure mechanism acting at the usage condition is the same as that at the accelerated conditions,
the compatibility of the disk and drive combination will affect the disk's initial recording quality and the resulting archival test outcome,
a hardware and software system needed to read the disk will be available at the time the retrieval of the information is attempted,
the recorded format will be recognizable and interpretable by the reading software.

### 7.1.3 Data Error

Of all specimen media, the data errors shall be measured in the disk testing locations as defined in 7.5. For each sample the Maximum Data Error shall be determined.

Each DVD-R/RW, +R/+RW disk will have its Maximum PI Sum 8 (Max PI Sum 8) determined.
Each DVD-RAM disk will have its Maximum Byte Error rate (Max BER) determined.
Each CD-R/RW disk will have its Maximum C1 Ave 10 (Max C1 Ave 10) determined.
Data collected at each time interval for each individual disk are then used to determine the predicted time to failure for that disk at that stress condition.

### 7.1.3.1 PI Sum 8

Per ISO/IEC 16448:2002, a row in an ECC block that has at least 1 byte in error constitutes a PI error. PI Sum 8 is measured over 8 ECC blocks in any 8 consecutive ECC blocks. The total number of PI errors, also called PI Sum 8, before error correction shall not exceed 280.

### 7.1.3.2 BER

The number of erroneous symbols shall be measured in any consecutive 32 ECC blocks in the first pass of the decoder before correction. The BER is the number of erroneous symbols divided by the total number of symbols included in the 32 consecutive ECC blocks. The maximum value of the BER measured over the area specified in 7.5 shall not exceed $10^{-3}$.

### 7.1.3.3 C1 Ave 10

IEC 60908:1999 specifies that the BLER averaged over any 10 seconds shall be less than $3 \times 10^{-2}$. At the standard (1X) data transfer rate, the total number of blocks per second entering the C1-decoder is 7350 .

Thus, the number of C 1 errors per second before error correction which is averaged over any 10 seconds, called C1 Ave 10, shall not exceed 220.

### 7.1.4 Data Quality

Data quality is checked by plotting the median rank of the estimated time to failure values with a best-fit line for each stress condition. The lines are then checked for reasonable parallelism.

### 7.1.5 Regression

The log predicted time to failure values shall be calculated using linear regression.
Multiple linear regression is used for the Eyring Method and linear regression is used for the Arrhenius Method.

### 7.2 Test specimen

The disk sample set shall represent the construction, materials, manufacturing process, quality and variation of the final process output.

Consideration shall be made to shelf life. Disks with longer shelf time before recording and testing may impact test results. Shelf time shall be representative of normal usage.

### 7.3 Recording conditions

Before media are entered into accelerated aging tests, they shall be recorded as optimally as is practicable, according to the descriptions given in the related standard. OPC (optimum power control) during the writing process shall serve as the method to achieve minimum data errors. It is generally assumed that optimallyrecorded media will yield the longest predicted lifetime. Media is deemed acceptable for entry into the aging tests when their data errors and all other media parametric specifications are found to be within their respective standard's specification limits.

The choice of recording hardware is at the discretion of the recording party. It may be either commercial drivebased or speciality recording tester based. It shall be capable of producing recordings that meet all specifications.

The recording speed used for testing shall be reported.
NOTE It is expected that lifetime of data on a disk may be affected by recording conditions including recording speed.

### 7.3.1 Recording test environment

When performing the recordings, the air immediately surrounding the media shall have the following properties:
temperature: $\quad 23^{\circ} \mathrm{C}$ to $35^{\circ} \mathrm{C}$
relative humidity: $\quad 45 \%$ to $55 \%$
atmospheric pressure: 60 kPa to 106 kPa
No condensation on the disk shall occur. Before testing, the disk shall be conditioned in this environment for 48 hrs minimum. It is recommended that, before testing, the entrance surface be cleaned according to the instructions of the manufacturer of the disk.

### 7.3.2 Recording method

Specimen disks shall be recorded in a single session and finalized.

### 7.4 Playback conditions

### 7.4.1 Playback tester

All media shall be read by the playback tester as specified in each of the medium's standard and at their specified test conditions.

Specimen media shall be read as described in the format standards identified in Clause 3.

### 7.4.2 Playback test environment

When measuring the data errors, the air immediately surrounding the disk shall have the following properties:

```
temperature: }\quad2\mp@subsup{3}{}{\circ}\textrm{C}\mathrm{ to }35\mp@subsup{5}{}{\circ}\textrm{C
relative humidity: 45 % to 55 %
atmospheric pressure: 60 kPa to 106 kPa
```

Unless otherwise stated, all tests and measurements shall be made in this test environment.

### 7.4.3 Calibration

The test equipment should be calibrated as prescribed by its manufacturer using calibration disks approved by said manufacturer and as needed before disk testing. A control disk should be maintained at ambient conditions and its data error should be measured at the same time the stressed disks are measured, both initially and after each stress sub interval.

The mean and standard deviation of the control disk shall be established by collecting at least five measurements. Should any individual data error differ from the mean by more than three times the standard deviation, the problem shall be corrected and all data collected since the last valid control point shall be remeasured.

### 7.5 Disk testing locations

### 7.5.1 Rigorous stress condition testing

All data areas on a disk shall be tested.

### 7.5.2 Basic stress condition testing

Testing locations shall be a minimum of three bands spaced evenly from the inner, middle and outer radius locations on the disk as indicated in Table 1. The total testing area shall represent a minimum of $5 \%$ of the disk capacity. For DVDs and $+\mathrm{R} /+\mathrm{RW}$ disks, each of the three test bands shall have more than 750 ECC blocks for 80 mm disks, and 2400 ECC blocks for 120 mm disks. For CDs, each of the three test bands shall have more than 5900 sectors.

Table 1 - Nominal radii of the three test bands (Unit; mm)

|  | DVD- R / RW, +R / +RW disk <br> (Single Layer / Dual Layer) |  | DVD- RAM disk |  | CD-R/RW disk |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 80 mm | 120 mm | 80 mm | 120 mm | 120 mm |
|  | 25,0 | 25,0 | $24,1-25,0$ | $24,1-25,0$ | 25,0 |
| Band 2 | 30,0 | 40,0 | $29,8-30,8$ | $39,4-40,4$ | 40,0 |
| Band 3 | 35,0 | 55,0 | $34,6-35,6$ | $54,9-55,8$ | 55,0 |

## 8 Accelerated stress test

### 8.1 General

Accelerated stress testing is used in order to estimate the lifetime of the optical disk. All information needed for this testing is provided in this document.

### 8.2 Stress conditions

### 8.2.1 General

Stress conditions for this test method are increases in temperature and relative humidity (RH). The stress conditions are intended to accelerate the chemical reaction rate from what would occur normally at ambient storage or usage conditions. The chemical reaction is considered to be degradation in some desired material property that eventually leads to disk failure.

Regarding use of the Eyring Method, five stress conditions for the Rigorous stress condition testing, and the minimum number of specimens for those stress conditions that shall be used, are shown in Table 2. Four stress conditions for the Basic stress condition testing, and the minimum numbers of specimens are also shown in Table 3. Additional specimens and conditions may be used, if desired for improved precision.

Regarding use of the Arrhenius Method, stress conditions are given in Table C. 1 and Table C. 2 in Annex C.
The total time for each stress condition as given in Table 2 and Table 3 is divided into five and four equal incubation sub-intervals respectively. The temperature and relative humidity ( RH ) during each incubation subinterval shall be controlled as given in Table 4 and shown in Figure 1. All specimens shall be measured after each sub-interval of incubation.

Table 2 - Rigorous stress conditions for use with the Eyring Method

| Test cell <br> number | Test stress <br> condition <br> (incubation) |  | Number of <br> specimens | Maximum <br> incubation <br> sub-interval <br> time | Minimum <br> total <br> incubation <br> time | Intermediate <br> RH | Minimum <br> equilibration <br> duration time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temp ( ${ }^{\circ} \mathrm{C}$ ) | $\% \mathrm{RH}$ |  | hours | hours | $\% \mathrm{RH}$ | hours |
|  | 85 | 80 | 20 | 300 | 1500 | 30 | 7 |
| B | 85 | 70 | 20 | 400 | 2000 | 30 | 6 |
| C | 85 | 60 | 20 | 600 | 3000 | 30 | 5 |
| D | 75 | 80 | 20 | 600 | 3000 | 32 | 8 |
| E | 65 | 80 | 30 | 800 | 4000 | 35 | 9 |

Table 3 - Basic stress conditions for use with the Eyring Method

| Test cell <br> number | Test stress <br> condition <br> (incubation) |  | Number of <br> specimens | Maximum <br> incubation <br> subinterval <br> time | Minimum <br> total <br> incubation <br> time | Intermediate <br> RH | Minimum <br> equilibration <br> duration <br> time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temp $\left({ }^{\circ} \mathrm{C}\right)$ | $\% \mathrm{RH}$ |  | hours | hours | $\% \mathrm{RH}$ | hours |
|  | 85 | 80 | 20 | 250 | 1000 | 30 | 7 |
| B | 85 | 70 | 20 | 250 | 1000 | 30 | 6 |
| C | 65 | 80 | 20 | 500 | 2000 | 35 | 9 |
| D | 70 | 75 | 30 | 625 | 2500 | 33 | 11 |

NOTE Incubation duration should be decided according to media characteristic.

### 8.2.2 Temperature ( T )

The temperature levels chosen for this test plan are based on the following:
There shall be no change of phase within the test system over the test-temperature range. This restricts the temperature to greater than $0^{\circ} \mathrm{C}$ and less than $100^{\circ} \mathrm{C}$,

The temperature shall not be so high that plastic deformation occurs anywhere within the disk structure.
The typical substrate material used for media is polycarbonate (glass transition temperature $\sim 150^{\circ} \mathrm{C}$ ). The glass transition temperature of other layers may be lower. Experience with high-temperature testing of DVDs, $+\mathrm{R} /+\mathrm{RW}$ disks and CD disks indicates that an upper limit of $85^{\circ} \mathrm{C}$ is practical for most applications.

### 8.2.3 Relative humidity (RH)

Experience indicates that $80 \%$ RH is the generally accepted upper limit for control within most accelerated test cells.

### 8.2.4 Incubation and Ramp Profiles

The relative humidity transition (ramp) profile is intended to avoid moisture condensation on the substrate, minimize substantial moisture gradients in the substrate and to end at ramp-down completion with the substrate equilibrated to the ambient condition. This is accomplished by varying the moisture content of the chamber only at the stress incubation temperature, and allowing sufficient time for equilibration during the ramp down based on the diffusion coefficient of water in polycarbonate.

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Table 4 - T and RH transition (ramp) profile for each incubation sub-interval

| Process step | Temperature ${ }^{\circ} \mathrm{C}$ | Relative humidity $\%$ | Duration hours |
| :---: | :---: | :---: | :---: |
| Start | at $T_{\text {amb }}$ | at $R H_{\text {amb }}$ | - |
| T, RH ramp | to $T_{\text {inc }}$ | to $R H_{\text {int }}$ | $1,5 \pm 0,5$ |
| RH ramp | at $T_{\text {inc }}$ | to $R H_{\text {inc }}$ | $1,5 \pm 0,5$ |
| Incubation | at $T_{\text {inc }}$ | at $R H_{\text {inc }}$ | See Table 2 |
| RH ramp | at $T_{\text {inc }}$ | to $R H_{\text {int }}$ | $1,5 \pm 0,5$ |
| Equilibration | at $T_{\text {inc }}$ | at $R H_{\text {int }}$ | See Table 2 |
| T, RH ramp | to $T_{\text {amb }}$ | to $R H_{\text {amb }}$ | $1,5 \pm 0,5$ |
| end | at $T_{\text {amb }}$ | at $R H_{\text {amb }}$ | - |

amb $=$ room ambient $T$ or $R H\left(T_{\text {amb }}\right.$ or $\left.R H_{\text {amb }}\right)$
inc $\quad=$ stress incubation $T$ or $R H$ ( $T_{\text {inc }}$ or $\left.R H_{\text {inc }}\right)$
int $\quad=$ intermediate relative humidity $\left(R H_{\text {int }}\right)$ that at $T_{\text {inc }}$ supports the same equilibrium moisture absorption in polycarbonate as that supported at $T_{\text {amb }}$ and $R H_{\text {amb }}$


Figure 1 - Graph of typical transition (ramp) profile

### 8.3 Measuring Time intervals

For data collection, PI Sum 8 (DVD-R, DVD-RW, +R, +RW), BER (DVD-RAM), or C1 Ave 10 (CD-R, CD-RW), measurements for each disk will occur: 1) before disk exposure to any stress condition to determine its baseline measurement and 2) after each sub-interval of incubation. The length of time for intervals is dependent on the severity of the stress condition.

Using each disk's regression equation, the failure time for each disk shall then be computed for the stress condition it was exposed to.

### 8.4 Stress Conditions Design

Table 2 for the Rigorous stress conditions and Table 3 for the Basic stress conditions specify the temperatures, relative humidities, Maximum Incubation sub-intervals, minimum total incubation time, and minimum number of specimens for each stress condition. A separate group of specimens shall be used for each stress condition.

All temperatures shall be maintained within $\pm 2^{\circ} \mathrm{C}$ of the target temperature; all relative humidities shall be maintained within $\pm 3 \% \mathrm{RH}$ of the target relative humidity.

The intermediate relative humidity in Table 2 and Table 3 are calculated assuming $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ ambient conditions. If the ambient is different, the intermediate relative humidity to be used is calculated using the equation:

$$
R H_{\mathrm{int}}=\frac{0,24+0,0037 \times T_{\mathrm{amb}}}{0,24+0,0037 \times T_{\mathrm{inc}}} \times R H_{\mathrm{amb}}
$$

where: $T_{\text {amb }}$ and $T_{\text {inc }}$ are the ambient and incubation temperature in units of ${ }^{\circ} \mathrm{C}$;
$R H_{\text {amb }}$ is the ambient relative humidity;
$R H_{\text {int }}$ is the intermediate relative humidity.
The stress conditions tabulated in Table 2, Table 3 and Table 4 offer sufficient combinations of temperature and relative humidity to satisfy the mathematical requirements of the Eyring Method to demonstrate linearity of either Max PI Sum 8, Max BER, or Max C1 Ave 10, or their logs respectively, versus time, and to produce a satisfactory confidence level to make a meaningful conclusion.

### 8.5 Media Orientation

Media subjected to this test method shall be maintained during incubation in a vertical position with a minimum of 2 mm separation between disks to allow air flow between disks and to minimize deposition of debris on disk surfaces, which could negatively influence the data error measurements.

## 9 Lifetime Estimation

### 9.1 Time to failure

All disks subjected to stress conditions shall have their time to failure calculated at the stress condition they have been subjected to. Failure criteria values are: Max PI Sum 8 exceeding 280 for DVD-R/RW, +R/+RW, Max BER exceeding $10^{-3}$ for DVD-RAM and Max C1 Ave 10 exceeding 220 for CD-R/-RW.

Material degradation manifests itself as data errors in the disk, providing a relationship between disk errors and material degradation. The chemical changes are generally expected to cause test data to have a
distribution that follows an exponential function over time. Therefore, test values of: PI Sum 8, BER or C1 Ave 10 as functions of time are expected to exhibit an exponential distribution.

The best function fitting an error trend can be found by regression of the test data against time, for example, with a least squares fit. The time to failure per disk type can be calculated using the error trend function and the failure criteria.

### 9.2 Accelerated Aging Test Methods

### 9.2.1 Eyring acceleration model (Eyring Method)

Using the Eyring model, the following equation is derived from the laws of thermodynamics and can be used to handle the two critical stresses of temperature and relative humidity.

$$
t=A T^{a} e^{\Delta H / k T} e^{(B+C / T) \times R H}
$$

where
$t \quad$ is the time to failure;
$A$ is the pre-exponential time constant;
$T^{a}$ is the pre-exponential temperature factor;
$\Delta H \quad$ is the activation energy per molecule;
$k \quad$ is the Boltzmann's constant ( $1,3807 \times 10^{-23} \mathrm{~J} /$ molecule degree K );
$T \quad$ is the temperature (in Kelvin);
$B, C$ are the $R H$ exponential constants;
$R H$ is the relative humidity;
For the temperature range used in this test method, " $a$ " and " $C$ " shall be set to zero. The Eyring model equation then reduces to the following equation.

$$
\begin{aligned}
& t=A e^{\Delta H / k T} e^{B \times R H} \\
& \text { or, } \ln (t)=\ln (A)+\frac{\Delta H}{k T}+B \times R H
\end{aligned}
$$

### 9.2.2 Arrhenius accelerated model (Arrhenius Method)

The Arrhenius Method uses only temperature stress for accelerated aging.
The time to failure is assumed to be governed by the following Arrhenius model equation.

$$
\begin{aligned}
& t=A e^{\Delta H / k T} \\
& \ln (t)=\ln (A)+\frac{\Delta H}{k T}
\end{aligned}
$$

### 9.3 Data Analysis

Data analysis is contained in the following Annexes:
Annex A: Outline of Media Life Estimation Method and Data Analysis Steps
Annex B: Media Life Estimation for the Controlled Storage Condition (Eyring Method)
Annex C: Media Life Estimation for the Harsh Storage Condition (Arrhenius Method)
Annex D: Interval Estimation for $B_{5}$ Life using Maximum Likelihood

### 9.4 Result of Estimated Media Life

Estimated lifetime based on the data analysis shall be reported as follows.
(1) Number and title of this standard
(2) Ambient storage condition for lifetime estimation
$25^{\circ} \mathrm{C} / 50 \%$ RH (Controlled storage condition) or $30^{\circ} \mathrm{C} / 80 \%$ RH (Harsh storage condition)
(3) Stress and testing condition

Rigorous stress condition testing or Basic stress condition testing
(4) The recording speed used for testing shall be reported. (see 7.3)
(5) $B_{50}$ Life, $B_{5}$ Life and $95 \%$ lower confidence bound of $B_{5}$ Life (= ( $B_{5}$ Life) $)$

NOTE In case a more precise analysis is required or a large estimate $\hat{\sigma}$ is found, the $95 \%$ lower confidence bound of $B_{5}$ Life should be computed according to annex $D$.

## Annex A

(normative)

## Outline of Media Life Estimation Method and Data Analysis Steps

## A. 1 Data analysis for media life estimation

## A.1.1 Assumptions for data analysis

Data analysis for lifetime estimation is based on the following assumptions.

- The lifetime of data recorded on an optical disk has a lognormal distribution.
- The Eyring Method is used for the Controlled storage condition ( $25^{\circ} \mathrm{C}, 50 \% \mathrm{RH}$ ). (see Annex B)
- The Arrhenius method is used for the Harsh storage condition ( $30^{\circ} \mathrm{C}$, $80 \% \mathrm{RH}$ ). (see Annex C)
A.1.2 Lognormal model and point estimation of $\ln \hat{B}_{5}$ and $\ln \hat{B}_{50}$

As lifetime $t$ is distributed with lognormal distribution $L N\left(\mu, \sigma^{2}\right)$, log lifetime $y(=\ln t)$ follows normal distribution $N\left(\mu, \sigma^{2}\right)$, where $\mu$ and $\sigma^{2}$ are the expected values of $y$ and variance, respectively.

$$
\begin{aligned}
y & =\mu(\mathbf{x})+\sigma \cdot z \\
& =\beta_{0}+\beta_{1} x_{1}+\beta_{2} x_{2}+\sigma \cdot z
\end{aligned}
$$

$z$ denotes percentile of $N\left(0, \sigma^{2}\right)$, and $\beta_{0}=\ln A, \beta_{1}=\Delta H / k, \beta_{2}=B$.
The $p$ percentile of the lifetime distribution, or $B_{P}$ Life, is widely used in reliability engineering. The point estimation of $\ln B_{p}$ is described as

$$
\ln \hat{B}_{p}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{1}+\hat{\beta}_{2} x_{2}+z_{p / 100} \hat{\sigma}
$$

Then the point estimates of the 5 percentile and 50 percentile of the lifetime distribution are given by

$$
\begin{aligned}
& \ln \hat{B}_{5}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}-1,64 \hat{\sigma} \\
& \ln \hat{B}_{50}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20} \\
& \text { where, }\left\{x_{10}, x_{20}\right\} \text { denotes the Controlled storage condition }\left(25^{\circ} \mathrm{C} \text { and } 50 \% \mathrm{RH}\right)
\end{aligned}
$$

## A.1.3 Interval estimation for optical disk

For interval estimation of $\ln \hat{B}_{p}$ for an optical disk, one may consider only the lower bound. (100- $\alpha$ ) $\%$ lower confidence bound of $\log$ lifetime $\ln \hat{B}_{p}$ is given by the following equation.

$$
\begin{aligned}
& \left.\left(\ln \hat{B}_{p}\right)_{L}=\ln \hat{B}_{p}+z_{\alpha / 100} \sqrt{\operatorname{Var}\left[\ln \hat{B}_{p}\right]}\right) \\
& \quad \text { where, } \operatorname{Var}\left\lfloor\ln \hat{B}_{p}\right\rfloor \text { denotes variance of } \ln \hat{B}_{p}(\text { see Annex D) }
\end{aligned}
$$

## ecma

When $\hat{\sigma}$ is relatively small, we can put $\sqrt{\operatorname{Var}\left[\ln \hat{B}_{p}\right]} \cong \hat{\sigma}$. Then the $95 \%$ lower confidence bound of $B_{5}$ Life becomes as follows.

$$
\begin{aligned}
\left(B_{5} \text { Life }\right)_{\mathrm{L}} & =\left(\exp \left(\ln \hat{B}_{5}\right)\right)_{L}=\exp \left(\ln \hat{B}_{5}-1.64 \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right]}\right) \\
& \cong \exp \left(\ln \hat{B}_{5}-1.64 \hat{\sigma}\right)
\end{aligned}
$$

NOTE In case a more precise analysis is required or a larger estimated $\hat{\sigma}$ is found, the $95 \%$ lower confidence bound of $B_{5}$ should be analyzed according to Annex D.

## A.1.4 Estimation of $\beta$ and $\sigma$ using the least squares method

The multiple linear regression model for $i$ th specimen is described as follows.

$$
y_{i}=\beta_{0}+\beta_{1} x_{1 i}+\beta_{2} x_{2 i}+\varepsilon_{i} \quad(i=1 \sim n)
$$

where, $\varepsilon_{i}$ denotes errors, and $n$ denotes total number of specimens.

The estimate $\hat{y}_{i}$ is given as

$$
\hat{y}_{i}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{1 i}+\hat{\beta}_{2} x_{2 i} .
$$

Also, the sum of the squared residual errors $S e$ is computed as

$$
S e=\sum_{i=1}^{n}\left(y_{i}-\hat{y}_{i}\right)^{2} .
$$

The regression coefficients of $\hat{y}_{i}$ can be obtained by applying the least squares method to Se . The estimates $\hat{\beta}_{0}, \hat{\beta}_{1}$ and $\hat{\beta}_{2}$ are obtained by solving 110 linear regression equations of group $\mathrm{A}, \mathrm{B}, \mathrm{C}, \mathrm{D}$ and E .
The estimate $\hat{\sigma}^{2}$ of variance is given as follows.

$$
\hat{\sigma}^{2}=\frac{S e}{(n-2-1)}=\frac{\sum\left(y_{i}-\hat{y}_{i}\right)^{2}}{(n-2-1)}
$$

where $n-2-1$ is the number of degrees of freedom.
The estimated regression coefficients $\hat{\beta}_{0}, \hat{\beta}_{1}$ and $\hat{\beta}_{2}$ and variance of residual errors $\hat{\sigma}_{2}$ are obtained using regression analysis of statistics software tools.
$B_{50}$ Life, $B_{5}$ Life and the $95 \%$ lower confidence bound of $B_{5}$ Life are described as follows.

$$
\begin{aligned}
B_{50} \text { Life } & =\exp \left(\ln \hat{B}_{50}\right) \\
& =\exp \left(\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}\right) \\
B_{5} \text { Life } & =\exp \left(\ln \hat{B}_{5}\right) \\
& =\exp \left(\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}-1,64 \hat{\sigma}\right)
\end{aligned}
$$

where, $\left\{x_{10}, x_{20}\right\}$ denotes the Controlled storage condition ( $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ )

Also, $95 \%$ lower confidence bound of $B_{5}$ Life becomes
$\left(B_{5} \text { Life }\right)_{\mathrm{L}} \cong \exp \left(\ln \hat{B}_{5}-1.64 \hat{\sigma}\right)$, when $\hat{\sigma}$ is relatively small. (see A.1.3)

## A. 2 Data analysis steps for lifetime estimation

The following is an outline of steps to estimate the media lifetime using the least squares method for the Eyring Method, as a function of ambient temperature and relative humidity.

1. For each specimen, ordered by increasing time to failure values, compute (via linear regression) the predicted time to failure.
2. (Steps 2 and 3 are for data quality check)

For each stress condition, the specimens are ordered by increasing time to failure values in order to determine the median rank of each specimen.
3. Plot the median rank versus time to failure on a lognormal graph. Verify that the fitting lines for all stress conditions are reasonably parallel to one another.
NOTE In the case where the fitting lines are not determined to be reasonably parallel, the assumptions made in Clause 7.1.2 shall be checked.
4. Multiple regression coefficients and the standard error can be calculated using the least squares method across all data of the log failure times, which were obtained at the five or four stress conditions. This calculation can be performed by multiple regression analysis of statistics software tools.
5. $\quad B_{50}$ Life, $B_{5}$ Life and $95 \%$ lower confidence bound of $B_{5}$ Life at the Controlled storage condition are calculated using the multiple regression coefficients and standard error.

For the conventional acceleration factor method, in addition to above steps 1 to 3 , following steps 4 to 7 are used
4. Calculate regression coefficients using the log mean failure time.
5. Calculate acceleration factors from the difference between the estimated log mean at each stress condition.
6. Calculate the normalized time to failure at the ambient condition for each specimen group using the acceleration factors, and plot these data on a lognormal graph.
7. $B_{50}$ Life, $B_{5}$ Life and $95 \%$ lower confidence bound of $B_{5}$ Life at the Controlled storage condition are calculated using $\hat{\mu}$ and $\hat{\sigma}$ obtained from the fitting line.

NOTE Data analysis steps using the Arrhenius Method are almost the same as the Eying Method. Single regression for Harsh storage temperature can be used for the Arrhenius Method.

## Annex B

 (normative)
## Media Life Estimation for the Controlled Storage Condition (Eyring method)

In this annex, two media life estimation methods by the least squares method using all data and the conventional acceleration factor method for the Rigorous stress condition testing are shown.

## B. 1 Data analysis and lifetime estimation using the least squares method

## Step 1

Determine the time to failure for each specimen at the stress applied following the procedure described below. Data Error to be measured is as defined in 7.1.3:

For DVD-R/-RW, +R/+RW: Max PI Sum 8
For DVD-RAM: Max BER
For CD-R/-RW: Max C1 Ave 10

Use the initial data errors measured prior to accelerated aging plus the data errors measured after each specified accelerated-aging incubation sub-interval.

For each specimen, a linear regression is performed with the In (measured data errors) as the dependent variable and time as the independent variable. The time to failure of the specimen is calculated from the slope and intercept of the regression as the time at which the specimen would have a Max PI Sum 8 of 280 , a Max BER of $10^{-3}$, or Max C1 Ave 10 of 220.

Table B. 1 shows calculations leading to an estimated time to failure from a hypothetical data set. The data for five stress conditions (Group A, Group B, Group C, Group D and Group E) are offered solely as an example of the mathematical methodology used in this test procedure.

## Step 2

For each stress condition, the specimens are ordered by increasing log time to failure values.
The median rank of the specimens is calculated using the estimate $(i-0,3) /(n+0,4)$, where $i$ is the time to failure order and $n$ is the total number of specimens at the stress condition.

Table B. 2 shows the ordered log time to failure and the median rank for the example data.

Table B. 1 - Ordered estimated time to failure for example data (Rigorous stress conditions)

| Order <br> Number | Group A | Group B | Group C | Group D | Group E |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $85^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ | $85^{\circ} \mathrm{C} / 70 \% \mathrm{RH}$ | $85^{\circ} \mathrm{C} / 60 \% \mathrm{RH}$ | $75^{\circ} \mathrm{C} / 80 \% R H$ | $65^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ |
| 1 | 429 | 613 | 864 | 1728 | 5455 |
| 2 | 451 | 640 | 913 | 1882 | 5730 |
| 3 | 476 | 649 | 915 | 1907 | 5908 |
| 4 | 484 | 675 | 945 | 1989 | 6114 |
| 5 | 493 | 679 | 951 | 2020 | 6326 |
| 6 | 495 | 696 | 993 | 2076 | 6431 |
| 7 | 501 | 703 | 994 | 2129 | 6544 |
| 8 | 512 | 709 | 998 | 2151 | 6632 |
| 9 | 521 | 719 | 1009 | 2180 | 6711 |
| 10 | 526 | 732 | 1014 | 2227 | 6779 |
| 11 | 534 | 739 | 1027 | 2277 | 6860 |
| 12 | 540 | 743 | 1030 | 2318 | 6935 |
| 13 | 542 | 747 | 1037 | 2352 | 7038 |
| 14 | 548 | 751 | 1049 | 2404 | 7108 |
| 15 | 557 | 766 | 1069 | 2443 | 7202 |
| 16 | 576 | 778 | 1080 | 2512 | 7285 |
| 17 | 579 | 785 | 1098 | 2589 | 7362 |
| 18 | 586 | 804 | 1125 | 2590 | 7454 |
| 19 | 618 | 856 | 1222 | 2776 | 7562 |
| 20 | 645 | 896 | 1249 | 2891 | 7569 |
| 21 |  |  |  |  | 7710 |
| 22 |  |  |  |  | 7827 |
| 23 |  |  |  |  | 7955 |
| 24 |  |  |  |  | 8067 |
| 25 |  |  |  |  | 8250 |
| 26 |  |  |  |  | 8405 |
| 27 |  |  |  |  | 8546 |
| 28 |  |  |  |  | 8700 |
| 30 |  |  |  |  |  |

Table B. 2 - Log time to failure and median rank for example data

| Group A | $85^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ |  |  |
| :---: | :---: | :---: | :---: |
| Order <br> Number | Time to <br> Failure(h) (=H) | $\ln (\mathrm{H})$ | Median <br> Rank |
| 1 | 429 | 6.0611 | 0.034 |
| 2 | 451 | 6.1115 | 0.083 |
| 3 | 476 | 6.1654 | 0.131 |
| 4 | 484 | 6.1822 | 0.181 |
| 5 | 493 | 6.2005 | 0.23 |
| 6 | 495 | 6.2046 | 0.279 |
| 7 | 501 | 6.2166 | 0.328 |
| 8 | 512 | 6.2383 | 0.377 |
| 9 | 521 | 6.2558 | 0.426 |
| 10 | 526 | 6.2653 | 0.475 |
| 11 | 534 | 6.2804 | 0.525 |
| 12 | 540 | 6.2913 | 0.574 |
| 13 | 542 | 6.2953 | 0.623 |
| 14 | 548 | 6.3063 | 0.672 |
| 15 | 557 | 6.3226 | 0.721 |
| 16 | 576 | 6.3561 | 0.77 |
| 17 | 579 | 6.3613 | 0.819 |
| 18 | 586 | 6.3733 | 0.869 |
| 19 | 618 | 6.4265 | 0.917 |
| 20 | 645 | 6.4693 | 0.966 |
|  |  |  |  |


| Group B | $85^{\circ} \mathrm{C} / 70 \% \mathrm{RH}$ |  |  |
| :---: | :---: | :---: | :---: |
| Order <br> Number | Time to <br> Failure(h) (=H) | $\ln (\mathrm{H})$ | Median <br> Rank |
| 1 | 613 | 6.4184 | 0.034 |
| 2 | 640 | 6.4615 | 0.083 |
| 3 | 649 | 6.4754 | 0.131 |
| 4 | 675 | 6.5147 | 0.181 |
| 5 | 679 | 6.5206 | 0.23 |
| 6 | 696 | 6.5453 | 0.279 |
| 7 | 703 | 6.5554 | 0.328 |
| 8 | 709 | 6.5639 | 0.377 |
| 9 | 719 | 6.5779 | 0.426 |
| 10 | 732 | 6.5958 | 0.475 |
| 11 | 739 | 6.6053 | 0.525 |
| 12 | 743 | 6.6107 | 0.574 |
| 13 | 747 | 6.6161 | 0.623 |
| 14 | 751 | 6.6214 | 0.672 |
| 15 | 766 | 6.6412 | 0.721 |
| 16 | 778 | 6.6567 | 0.77 |
| 17 | 785 | 6.6657 | 0.819 |
| 18 | 804 | 6.6896 | 0.869 |
| 19 | 856 | 6.7523 | 0.917 |
| 20 | 896 | 6.7979 | 0.966 |
| Mean | 734 | 6.5943 |  |


| Group C | $85^{\circ} \mathrm{C} / 60 \% \mathrm{RH}$ |  |  |
| :---: | :---: | :---: | :---: |
| Order <br> Number | Time to <br> Failure(h) (=H) | $\ln (\mathrm{H})$ | Median <br> Rank |
| 1 | 864 | 6.7616 | 0.034 |
| 2 | 913 | 6.8167 | 0.083 |
| 3 | 915 | 6.8189 | 0.131 |
| 4 | 945 | 6.8512 | 0.181 |
| 5 | 951 | 6.8575 | 0.23 |
| 6 | 993 | 6.9007 | 0.279 |
| 7 | 994 | 6.9017 | 0.328 |
| 8 | 998 | 6.9058 | 0.377 |
| 9 | 1009 | 6.9167 | 0.426 |
| 10 | 1014 | 6.9217 | 0.475 |
| 11 | 1027 | 6.9344 | 0.525 |
| 12 | 1030 | 6.9373 | 0.574 |
| 13 | 1037 | 6.9441 | 0.623 |
| 14 | 1049 | 6.9556 | 0.672 |
| 15 | 1069 | 6.9745 | 0.721 |
| 16 | 1080 | 6.9847 | 0.77 |
| 17 | 1098 | 7.0012 | 0.819 |
| 18 | 1125 | 7.0255 | 0.869 |
| 19 | 1222 | 7.1082 | 0.917 |
| 20 | 1249 | 7.1301 | 0.966 |
| Mean | 1029 | 6.9324 |  |


| Group D | $75^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ |  |  |
| :---: | :---: | :---: | :---: |
| Order <br> Number | Time to <br> Failure(h) (=H) | $\ln (\mathrm{H})$ | Median <br> Rank |
| 1 | 1728 | 7.4549 | 0.034 |
| 2 | 1882 | 7.5403 | 0.083 |
| 3 | 1907 | 7.5534 | 0.131 |
| 4 | 1989 | 7.5953 | 0.181 |
| 5 | 2020 | 7.6106 | 0.23 |
| 6 | 2076 | 7.6381 | 0.279 |
| 7 | 2129 | 7.6632 | 0.328 |
| 8 | 2151 | 7.6739 | 0.377 |
| 9 | 2180 | 7.6871 | 0.426 |
| 10 | 2227 | 7.7085 | 0.475 |
| 11 | 2277 | 7.7308 | 0.525 |
| 12 | 2318 | 7.7484 | 0.574 |
| 13 | 2352 | 7.7632 | 0.623 |
| 14 | 2404 | 7.7850 | 0.672 |
| 15 | 2443 | 7.8008 | 0.721 |
| 16 | 2512 | 7.8287 | 0.77 |
| 17 | 2589 | 7.8592 | 0.819 |
| 18 | 2590 | 7.8594 | 0.869 |
| 19 | 2776 | 7.9286 | 0.917 |
| 20 | 2891 | 7.9695 | 0.966 |
| Mean | 2272 | 7.7199 |  |


| Group E | $65^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ |  |  |
| :---: | :---: | :---: | :---: |
| Order <br> Number | Time to Failure(h) (=H) | $\ln (\mathrm{H})$ | Median Rank |
| 1 | 5455 | 8.6043 | 0.023 |
| 2 | 5730 | 8.6535 | 0.056 |
| 3 | 5908 | 8.6841 | 0.089 |
| 4 | 6114 | 8.7183 | 0.122 |
| 5 | 6326 | 8.7525 | 0.155 |
| 6 | 6431 | 8.7689 | 0.188 |
| 7 | 6544 | 8.7864 | 0.22 |
| 8 | 6632 | 8.7997 | 0.253 |
| 9 | 6711 | 8.8115 | 0.286 |
| 10 | 6779 | 8.8216 | 0.319 |
| 11 | 6860 | 8.8335 | 0.352 |
| 12 | 6935 | 8.8443 | 0.385 |
| 13 | 7038 | 8.8591 | 0.418 |
| 14 | 7108 | 8.8690 | 0.451 |
| 15 | 7202 | 8.8822 | 0.484 |
| 16 | 7285 | 8.8936 | 0.516 |
| 17 | 7362 | 8.9041 | 0.549 |
| 18 | 7454 | 8.9165 | 0.582 |
| 19 | 7562 | 8.9309 | 0.615 |
| 20 | 7569 | 8.9319 | 0.648 |
| 21 | 7710 | 8.9503 | 0.681 |
| 22 | 7827 | 8.9653 | 0.714 |
| 23 | 7955 | 8.9816 | 0.747 |
| 24 | 8067 | 8.9955 | 0.78 |
| 25 | 8250 | 9.0180 | 0.813 |
| 26 | 8405 | 9.0366 | 0.845 |
| 27 | 8546 | 9.0532 | 0.878 |
| 28 | 8700 | 9.0711 | 0.911 |
| 29 | 8953 | 9.0997 | 0.944 |
| 30 | 9452 | 9.1540 | 0.977 |
| Mean | 7296 | 8.8864 |  |

## Step 3

The data can be plotted in different ways. If lognormal graph paper is employed, the data is plotted with time to failure on the abscissa and median rank on the ordinate.

NOTE On most lognormal graph paper, the actual ordinate scale is the probability of failure, and the median rank is converted to the probability of failure by multiplying by 100.

Figure $B .1$ shows lognormal plots of specimen groups A, B, C, D and E from Table B.2. Each best fit straight line is drawn through the plotted data. If the lines are judged to be reasonably parallel, the assumption of equivalent log standard deviation applicable to the individual data sets is verified.

An estimate of the log standard deviation can be obtained from the graphical treatment of the failure data. First, for each stress, estimate the times corresponding to $15,9 \%$ and $84,1 \%$ failure based on the best-fit straight line through the time to failure data. The estimated log standard deviation $\hat{\sigma}$ is then calculated as follows.

$$
\hat{\sigma}=\left(\ln t_{0,841}-\ln t_{0,159}\right) / 2
$$



Figure B. 1 - Best fit lines of specimen group A, B, C, D and E on lognormal paper (Verify that the fitting lines for all stress conditions are reasonably parallel to one another)

The averaged log standard deviation estimate $\hat{\sigma}_{m}$ of five groups is then calculated as

$$
\begin{aligned}
\hat{\sigma}_{m} & =\left(\hat{\sigma}_{A}+\hat{\sigma}_{B}+\hat{\sigma}_{C}+\hat{\sigma}_{D}+\hat{\sigma}_{E}\right) / 5 \\
& =(0,1036+0,09759+0,09633+0,1407+0,1378) / 5=0,1152
\end{aligned}
$$

## Step 4

Table $B .3$ shows all 110 sample data points belonging to specimen groups $A, B, C, D$ and $E$ for regression analysis. The regression coefficients and error variance are calculated by applying the least squares method to 110 failure data that were obtained under the five stress conditions. Table B. 4 shows the result of
regression analysis of the statistics software tool. Residual error estimate $\hat{S} e$, variance estimate $\hat{\sigma}^{2}$, standard error estimate $\hat{\sigma}$, and regression coefficient estimates $\hat{\beta}_{0}, \hat{\beta}_{1}$ and $\hat{\beta}_{2}$ are quickly obtained. Other statistics tools also can be used for regression analysis.

NOTE The standard error estimate $\hat{\sigma}(=0,13169)$ at the controlled storage condition is fairly large in comparison with the averaged estimate $\hat{\sigma}_{m}$ of the five specimen groups. Variation in the best-fit lines among the five groups and the lognormal distributions of each group are among the anomalies that may affect the log standard error.

Table B. 3 - 110 sample data for regression analysis

| Number | $\ln \mathrm{t}$ | $x_{1}$ | $x_{2}$ |
| :---: | :---: | :---: | :---: |
| 1 | 6.061055 | 0.002792 | 80 |
| 2 | 6.111467 | 0.002792 | 80 |
| 3 | 6.165418 | 0.002792 | 80 |
| 4 | 6.182176 | 0.002792 | 80 |
| 5 | 6.200509 | 0.002792 | 80 |
| 6 | 6.204558 | 0.002792 | 80 |
| 7 | 6.216606 | 0.002792 | 80 |
| 8 | 6.238325 | 0.002792 | 80 |
| 9 | 6.255750 | 0.002792 | 80 |
| 10 | 6.265301 | 0.002792 | 80 |
| 11 | 6.280396 | 0.002792 | 80 |
| 12 | 6.291310 | 0.002792 | 80 |
| 13 | 6.295266 | 0.002792 | 80 |
| 14 | 6.306275 | 0.002792 | 80 |
| 15 | 6.322565 | 0.002792 | 80 |
| 16 | 6.356108 | 0.002792 | 80 |
| 17 | 6.361302 | 0.002792 | 80 |
| 18 | 6.373320 | 0.002792 | 80 |
| 19 | 6.426488 | 0.002792 | 80 |
| 20 | 6.469250 | 0.002792 | 80 |
| 1 | 6.418365 | 0.002792 | 70 |
| 2 | 6.461468 | 0.002792 | 70 |
| 3 | 6.475433 | 0.002792 | 70 |
| 4 | 6.514713 | 0.002792 | 70 |
| 5 | 6.520621 | 0.002792 | 70 |
| 6 | 6.545350 | 0.002792 | 70 |
| 7 | 6.555357 | 0.002792 | 70 |
| 8 | 6.563856 | 0.002792 | 70 |
| 9 | 6.577861 | 0.002792 | 70 |
| 10 | 6.595781 | 0.002792 | 70 |
| 11 | 6.605298 | 0.002792 | 70 |
| 12 | 6.610696 | 0.002792 | 70 |
| 13 | 6.616065 | 0.002792 | 70 |
| 14 | 6.621406 | 0.002792 | 70 |
| 15 | 6.641182 | 0.002792 | 70 |
| 16 | 6.656727 | 0.002792 | 70 |
| 17 | 6.665684 | 0.002792 | 70 |
| 18 | 6.689599 | 0.002792 | 70 |
| 19 | 6.752270 | 0.002792 | 70 |
| 20 | 6.797940 | 0.002792 | 70 |
| 1 | 6.761573 | 0.002792 | 60 |
| 2 | 6.816736 | 0.002792 | 60 |
| 3 | 6.818924 | 0.002792 | 60 |
| 4 | 6.851185 | 0.002792 | 60 |
| 5 | 6.857514 | 0.002792 | 60 |
| 6 | 6.900731 | 0.002792 | 60 |
| 7 | 6.901737 | 0.002792 | 60 |
| 8 | 6.905753 | 0.002792 | 60 |
| 9 | 6.916715 | 0.002792 | 60 |
| 10 | 6.921658 | 0.002792 | 60 |
| 11 | 6.934397 | 0.002792 | 60 |
| 12 | 6.937314 | 0.002792 | 60 |
| 13 | 6.944087 | 0.002792 | 60 |
| 14 | 6.955593 | 0.002792 | 60 |
| 15 | 6.974479 | 0.002792 | 60 |
| 16 | 6.984716 | 0.002792 | 60 |
| 17 | 7001246 | 0002792 | 60 |
| 18 | 7.025538 | 0.002792 | 60 |
| 19 | 7.108244 | 0.002792 | 60 |
| 20 | 7.130099 | 0.002792 | 60 |

Group A

Group B

Group C


Table B. 4 - Regression analysis results

| Regression coefficients |  |  | Sum of squared <br> residual errors | Standard deviation <br> of residual errors |
| :---: | :---: | :---: | :---: | :---: |
| $\hat{\beta}_{0}$ | $\hat{\beta}_{1}$ | $\hat{\beta}_{2}$ | $\hat{S}_{e}$ | $\hat{\sigma}$ |
| $-35,3479$ | 15777,96 | $-0,02979$ | 1,86350 | 0,13197 |

## Step 5

$\ln \hat{B}_{50}$ and $\ln \hat{B}_{5}$ at the Controlled storage condition ( $25{ }^{\circ} \mathrm{C} / 50 \% R H$ ) are obtained using the regression coefficient estimates $\hat{\beta}_{0}, \hat{\beta}_{1}$ and $\hat{\beta}_{2}$ and standard error estimate $\hat{\sigma}$ which were obtained in Step 4.

Then $B_{50}$ Life, $B_{5}$ Life and $95 \%$ lower confidence bound of $B_{5}$ Life at the Controlled storage condition ( $25^{\circ} \mathrm{C}$ $/ 50 \% \mathrm{RH}$ ) can be calculated using $\ln \hat{B}_{50}$ and $\ln \hat{B}_{5}$ (see A.1.3).

$$
\left.\begin{array}{rl}
\ln \hat{B}_{50} & =\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20} \\
& =-35,3479+15777,96 \times 0,003354-0,02979 \times 50 \\
& =16,0823 \\
B_{50} \text { Life } & =\exp (16.0823)=9648593 \text { hours (1101 years) } \\
\ln \hat{B}_{5} & =\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}-1.64 \hat{\sigma}=\ln \hat{B}_{50}-1,64 \hat{\sigma} \\
& =16,0823-1,64 \times 0,13197 \\
& =15,8659
\end{array}\right\}
$$

$95 \%$ lower confidence bound of $B_{5}$ Life: ( $B_{5}$ Life $)_{\llcorner }$

$$
\begin{aligned}
& =\left(\exp \left(\ln \hat{B}_{5}\right)\right)_{L}=\exp \left(\ln \hat{B}_{5}+z_{5 / 100} \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right]}\right) \cong \exp \left(\ln \hat{B}_{5}-1.64 \hat{\sigma}\right) \\
& =\exp (15,8659-1.64 \times 0,13197)=\exp (15,6495) \\
& =6258580 \text { hours ( } 714 \text { years })
\end{aligned}
$$

## B. 2 Data analysis and lifetime estimation using the conventional acceleration factor method (Step 4-7)

## Step 4

Table B. 5 shows log mean time to failure for each stress group A, B, C, D, and E (see Table B.2)

Table B. 5 - Log mean failure time for each stress condition

| Group | Log mean | Temp | $1 / \mathrm{T}$ | $\%$ RH |
| :---: | :---: | :---: | :---: | :---: |
| A | 6,2692 | 85 | 0,002792 | 80 |
| B | 6,5943 | 85 | 0,002792 | 70 |
| C | 6,9324 | 85 | 0,002792 | 60 |
| D | 7.7199 | 75 | 0,002872 | 80 |
| E | 8,8864 | 65 | 0,002957 | 80 |

To determine the coefficients $A, \Delta H / k$ and $B$ of the reduced Eyring equation, the regression analysis is done using five log mean values obtained at the temperature and relative humidity in Table B. 5

$$
\log \text { mean }_{i}=\ln (A)+\left(\frac{\Delta H}{k}\right) \times\left(\frac{1}{T_{i}}\right)+B \times R H_{i}+\varepsilon_{i}
$$

where, $i=1 \sim 5$
The estimate values are determined as follows.

$$
\begin{array}{ll}
\ln (\hat{A}) & =\hat{\beta}_{0}=-35,6889 \\
\Delta \hat{H} / k & =\hat{\beta}_{1}=15904,21 \\
\hat{B} & =\hat{\beta}_{2}=-0.029978
\end{array}
$$

## Step 5

The acceleration factors are calculated from the difference between estimated log mean at each stress condition and that at the controlled storage condition ( $25^{\circ} \mathrm{C} / 50 \% \mathrm{RH}$ ). They are listed in Table B. 6

Table B. 6 - Calculated lifetime and acceleration factors for each stress condition

| Stress condition | Calculated <br> lifetime |  |  | Acceleration <br> factor |
| :---: | :---: | :---: | :---: | :---: |
|  | $1 / \mathrm{T}$ | Ln (lifetime) | Lifetime (h) |  |
| $85^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ | 0,002792 | 6,3202 | 556 | 18685 |
| $85^{\circ} \mathrm{C} / 70 \% \mathrm{RH}$ | 0,002792 | 6,6199 | 750 | 13846 |
| $85^{\circ} \mathrm{C} / 60 \% \mathrm{RH}$ | 0,002792 | 6,9196 | 1012 | 10261 |
| $75^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ | 0,002872 | 7,5957 | 1990 | 5218 |
| $65^{\circ} \mathrm{C} / 80 \% \mathrm{RH}$ | 0,002957 | 8,9467 | 7682 | 1352 |
| $25^{\circ} \mathrm{C} / 50 \% \mathrm{RH}$ | 0,003354 | 16,1557 | 10383119 |  |

## Step 6

Using the acceleration factors on Table B.6, calculate normalized time to failure at $25{ }^{\circ} \mathrm{C} / 50 \% \mathrm{RH}$ for each specimen group $A, B, C, D$ and $E$. Table $B .7$ shows data for a composite lognormal plot. Figure B. 2 shows a lognormal plot using the composite data of Table B.7. From the fitting line for those data, the log mean $(\hat{\mu}=16,15)$ and standard deviation $(\hat{\sigma}=0,1324)$ can be obtained. These values are almost same as the values which were calculated in Table B.7.

Table B. 7 - Data for composite lognormal plot

| Time to Failure | Group | Normarized to $25^{\circ} \mathrm{C} / 50 \% \mathrm{RH}$ | Ln | Group | Accending | Order | Median Rank |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 429 | A | 8012443 | 15.89651 | E | 15.7432 | 1 | 0.0063 |
| 451 | A | 8426726 | 15.94692 | E | 15.79238 | 2 | 0.0154 |
| 476 | A | 8893839 | 16.00087 | E | 15.82297 | 3 | 0.0245 |
| 484 | A | 9044142 | 16.01763 | A | 15.8327 | 4 | 0.0335 |
| 493 | A | 9211476 | 16.03596 | E | 15.85725 | 5 | 0.0426 |
| 495 | A | 9248845 | 16.04001 | A | 15.88312 | 6 | 0.0516 |
| 501 | A | 9360953 | 16.05206 | E | 15.89141 | 7 | 0.0607 |
| 512 | A | 9566482 | 16.07378 | E | 15.90779 | 8 | 0.0697 |
| 521 | A | 9734643 | 16.0912 | B | 15.91875 | 9 | 0.0788 |
| 526 | A | 9828066 | 16.10075 | E | 15.92527 | 10 | 0.0879 |
| 534 | A | 9977542 | 16.11585 | A | 15.93707 | 11 | 0.0969 |
| 540 | A | 10087039 | 16.12676 | E | 15.93857 | 12 | 0.1060 |
| 542 | A | 10127018 | 16.13072 | E | 15.95041 | 13 | 0.1150 |
| 548 | A | 10239126 | 16.14173 | A | 15.95382 | 14 | 0.1241 |
| 557 | A | 10407287 | 16.15802 | E | 15.96054 | 15 | 0.1332 |
| 576 | A | 10762293 | 16.19156 | B | 15.96185 | 16 | 0.1422 |
| 579 | A | 10818346 | 16.19675 | A | 15.97216 | 17 | 0.1513 |
| 586 | A | 10949138 | 16.20877 | E | 15.97237 | 18 | 0.1603 |
| 618 | A | 11547043 | 16.26194 | B | 15.97581 | 19 | 0.1694 |
| 645 | A | 12051526 | 16.3047 | A | 15.97621 | 20 | 0.1784 |
| 613 | B | 8487790 | 15.95414 | E | 15.98325 | 21 | 0.1875 |
| 640 | B | 8861640 | 15.99724 | A | 15.98825 | 22 | 0.1966 |
| 649 | B | 8986257 | 16.01121 | C | 15.99069 | 23 | 0.2056 |
| 675 | B | 9346261 | 16.05049 | E | 15.99799 | 24 | 0.2147 |
| 679 | B | 9401646 | 16.0564 | E | 16.00789 | 25 | 0.2237 |
| 696 | B | 9637034 | 16.08112 | A | 16.00997 | 26 | 0.2328 |
| 703 | B | 9733958 | 16.09113 | B | 16.01509 | 27 | 0.2418 |
| 709 | B | 9817036 | 16.09963 | B | 16.021 | 28 | 0.2509 |
| 719 | B | 9955499 | 16.11364 | E | 16.02108 | 29 | 0.2600 |
| 732 | B | 10135501 | 16.13155 | A | 16.0274 | 30 | 0.2690 |
| 739 | B | 10232425 | 16.14107 | E | 16.03248 | 31 | 0.2781 |
| 743 | B | 10287811 | 16.14647 | A | 16.03695 | 32 | 0.2871 |
| 747 | B | 10343196 | 16.15184 | E | 16.043 | 33 | 0.2962 |
| 751 | B | 10398581 | 16.15718 | B | 16.04573 | 34 | 0.3053 |
| 766 | B | 10606276 | 16.17696 | C | 16.04585 | 35 | 0.3143 |
| 778 | B | 10772431 | 16.1925 | C | 16.04804 | 36 | 0.3234 |
| 785 | B | 10869356 | 16.20146 | A | 16.05204 | 37 | 0.3324 |
| 804 | B | 11132436 | 16.22537 | E | 16.05542 | 38 | 0.3415 |
| 856 | B | 11852444 | 16.28804 | B | 16.05574 | 39 | 0.3505 |
| 896 | B | 12406296 | 16.33371 | A | 16.06296 | 40 | 0.3596 |
| 864 | C | 8865428 | 15.99767 | B | 16.06424 | 41 | 0.3687 |
| 913 | C | 9368213 | 16.05283 | A | 16.06691 | 42 | 0.3777 |
| 915 | C | 9388735 | 16.05502 | E | 16.0698 | 43 | 0.3868 |
| 945 | C | 9696562 | 16.08728 | E | 16.07077 | 44 | 0.3958 |
| 951 | C | 9758127 | 16.09361 | A | 16.07792 | 45 | 0.4049 |
| 993 | C | 10189086 | 16.13683 | B | 16.07824 | 46 | 0.4139 |
| 994 | C | 10199347 | 16.13783 | C | 16.0803 | 47 | 0.4230 |
| 998 | C | 10240390 | 16.14185 | C | 16.08663 | 48 | 0.4321 |
| 1009 | C | 10353260 | 16.15281 | E | 16.08918 | 49 | 0.4411 |
| 1014 | C | 10404565 | 16.15776 | A | 16.09421 | 50 | 0.4502 |
| 1027 | C | 10537957 | 16.17049 | B | 16.09616 | 51 | 0.4592 |
| 1030 | C | 10568740 | 16.17341 | E | 16.10424 | 52 | 0.4683 |
| 1037 | C | 10640566 | 16.18018 | B | 16.10568 | 53 | 0.4774 |
| 1049 | C | 10763697 | 16.19169 | D | 16.10888 | 54 | 0.4864 |
| 1069 | C | 10968915 | 16.21058 | B | 16.11108 | 55 | 0.4955 |
| 1080 | C | 11081785 | 16.22081 | B | 16.11645 | 56 | 0.5045 |
| 1098 | C | 11266482 | 16.23734 | E | 16.12047 | 57 | 0.5136 |
| 1125 | C | 11543526 | 16.26164 | B | 16.12179 | 58 | 0.5226 |
| 1222 | C | 12538835 | 16.34434 | A | 16.12776 | 59 | 0.5317 |
| 1249 | C | 12815879 | 16.3662 | C | 16.12984 | 60 | 0.5408 |


| Time to Failure | Group | Normarized to $25^{\circ} \mathrm{C} / 50 \% \mathrm{RH}$ | Ln | Group | Accending | Order | Median Rank |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1728 | D | 9019222 | 16.01487 | C | 16.13085 | 61 | 0.5498 |
| 1882 | D | 9822901 | 16.10023 | A | 16.13295 | 62 | 0.5589 |
| 1907 | D | 9952244 | 16.11331 | E | 16.13446 | 63 | 0.5679 |
| 1989 | D | 10378769 | 16.15527 | C | 16.13487 | 64 | 0.5770 |
| 2020 | D | 10538914 | 16.17059 | B | 16.14156 | 65 | 0.5861 |
| 2076 | D | 10831952 | 16.19801 | A | 16.14497 | 66 | 0.5951 |
| 2129 | D | 11107416 | 16.22312 | C | 16.14583 | 67 | 0.6042 |
| 2151 | D | 11227376 | 16.23387 | C | 16.15077 | 68 | 0.6132 |
| 2180 | D | 11376638 | 16.24707 | E | 16.15688 | 69 | 0.6223 |
| 2227 | D | 11622800 | 16.26848 | B | 16.15711 | 70 | 0.6313 |
| 2277 | D | 11884935 | 16.29078 | C | 16.16351 | 71 | 0.6404 |
| 2318 | D | 12095230 | 16.30832 | B | 16.16606 | 72 | 0.6495 |
| 2352 | D | 12275916 | 16.32315 | C | 16.16643 | 73 | 0.6585 |
| 2404 | D | 12546937 | 16.34499 | C | 16.1732 | 74 | 0.6676 |
| 2443 | D | 12746870 | 16.3608 | E | 16.17549 | 75 | 0.6766 |
| 2512 | D | 13106751 | 16.38864 | C | 16.18471 | 76 | 0.6857 |
| 2589 | D | 13512304 | 16.41911 | B | 16.18998 | 77 | 0.6947 |
| 2590 | D | 13514883 | 16.4193 | E | 16.19213 | 78 | 0.7038 |
| 2776 | D | 14484070 | 16.48856 | D | 16.19424 | 79 | 0.7129 |
| 2891 | D | 15088313 | 16.52943 | A | 16.19814 | 80 | 0.7219 |
| 5455 | E | 7372725 | 15.8133 | C | 16.20359 | 81 | 0.7310 |
| 5730 | E | 7744402 | 15.86248 | D | 16.20732 | 82 | 0.7400 |
| 5908 | E | 7984979 | 15.89307 | E | 16.20999 | 83 | 0.7491 |
| 6114 | E | 8263399 | 15.92735 | C | 16.21383 | 84 | 0.7582 |
| 6326 | E | 8550584 | 15.96151 | C | 16.23036 | 85 | 0.7672 |
| 6431 | E | 8691841 | 15.9779 | E | 16.23865 | 86 | 0.7763 |
| 6544 | E | 8845106 | 15.99537 | A | 16.2409 | 87 | 0.7853 |
| 6632 | E | 8963504 | 16.00867 | D | 16.24928 | 88 | 0.7944 |
| 6711 | E | 9070276 | 16.02051 | B | 16.25265 | 89 | 0.8034 |
| 6779 | E | 9162595 | 16.03064 | C | 16.25465 | 90 | 0.8125 |
| 6860 | E | 9271658 | 16.04247 | D | 16.2646 | 91 | 0.8216 |
| 6935 | E | 9373024 | 16.05335 | D | 16.29202 | 92 | 0.8306 |
| 7038 | E | 9512234 | 16.06809 | E | 16.29289 | 93 | 0.8397 |
| 7108 | E | 9606843 | 16.07799 | B | 16.29832 | 94 | 0.8487 |
| 7202 | E | 9734449 | 16.09118 | D | 16.31713 | 95 | 0.8578 |
| 7285 | E | 9846068 | 16.10258 | D | 16.32788 | 96 | 0.8668 |
| 7362 | E | 9950138 | 16.1131 | C | 16.33736 | 97 | 0.8759 |
| 7454 | E | 10074481 | 16.12552 | D | 16.34108 | 98 | 0.8850 |
| 7562 | E | 10220441 | 16.1399 | C | 16.35921 | 99 | 0.8940 |
| 7569 | E | 10230357 | 16.14087 | D | 16.36249 | 100 | 0.9031 |
| 7710 | E | 10420478 | 16.15928 | D | 16.38479 | 101 | 0.9121 |
| 7827 | E | 10578610 | 16.17434 | D | 16.40233 | 102 | 0.9212 |
| 7955 | E | 10751609 | 16.19057 | D | 16.41716 | 103 | 0.9303 |
| 8067 | E | 10903080 | 16.20456 | D | 16.439 | 104 | 0.9393 |
| 8250 | E | 11150317 | 16.22698 | D | 16.45481 | 105 | 0.9484 |
| 8405 | E | 11359808 | 16.24559 | D | 16.48265 | 106 | 0.9574 |
| 8546 | E | 11550377 | 16.26223 | D | 16.51312 | 107 | 0.9665 |
| 8700 | E | 11758516 | 16.28009 | D | 16.51331 | 108 | 0.9755 |
| 8953 | E | 12100459 | 16.30875 | D | 16.58257 | 109 | 0.9846 |
| 9452 | E | 12774885 | 16.36299 | D | 16.62344 | 110 | 0.9937 |
|  |  | Mean | 16.15021 |  |  |  |  |
|  |  | Deviation | 0.131013 |  |  |  |  |



Figure B. 2 - Plot on lognormal paper for composite data

## Step 7

$B_{50}$ Life, $B_{5}$ Life and the $95 \%$ lower confidence of $B_{5}$ Life at the Controlled storage condition ( $25^{\circ} \mathrm{C} / 50$ $\% \mathrm{RH}$ ) can be calculated as follows.

$$
B_{50} \text { Life }=\exp (\hat{\mu})=\exp (16,15)=10324187 \text { hours (1 } 179 \text { years) }
$$

$$
B_{5} \text { Life }=\exp (\hat{\mu}-1.64 \hat{\sigma})=\exp (16,15-1,64 \times 0,1324)=\exp (15,933)
$$

$=8309118$ hours (949 years)
$95 \%$ lower confidence bound of $B_{5}$ Life: ( $B_{5}$ Life $)_{\llcorner }$

$$
\begin{aligned}
& \left.=\left(\exp \left(\ln \hat{B}_{5}\right)\right)_{L}=\exp \left(\ln \hat{B}_{5}+z_{5 / 100} \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right.}\right]\right) \cong \exp \left(\ln \hat{B}_{5}-1.64 \hat{\sigma}\right) \\
& =\exp (15,933-1.64 \times 0,1324)=\exp (15,716) \\
& =6687348 \text { hours }(763 \text { years })
\end{aligned}
$$

## Annex C (normative)

## Media Life Estimation for the Harsh Storage Condition (Arrhenius method)

## C. 1 Stress conditions and data analysis steps for the Arrhenius method

Here, a test method is shown for the Harsh storage condition at higher temperature and relative humidity than that of the Controlled storage condition ( $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ ).

This test method follows the scope in this document, which is based on an environment of $30^{\circ} \mathrm{C}$ and $80 \%$ RH representing the most severe condition in which users handle and store the optical media. This test method also uses a different stress test design that makes possible the use of the Arrhenius method.

The same assumptions and data analysis method apply for the ambient storage condition, stress design, and Eyring equation. The controlled storage condition of $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ is replaced by an expected harsher user environment of $30^{\circ} \mathrm{C}$ and $80 \% \mathrm{RH}$.

Table C. 1 and C. 2 show summary of stress design for the Arrhenius Method.

Table C. 1 - Rigorous stress condition testing for use with the Arrhenius Method

| Test cell <br> number | Test stress <br> condition <br> (incubation) |  | Number of <br> specimens | Maximum <br> incubation <br> sub-interval <br> time | Minimum <br> total <br> incubation <br> time | Intermediate <br> RH | Minimum <br> equilibration <br> duration time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temp $\left({ }^{\circ} \mathrm{C}\right)$ | $\% \mathrm{RH}$ |  | hours | hours | $\% \mathrm{RH}$ | hours |
| A | 85 | 80 | 20 | 300 | 1500 | 30 | 5 |
| B | 80 | 80 | 20 | 400 | 2000 | 31 | 7 |
| C | 75 | 80 | 20 | 600 | 3000 | 32 | 8 |
| D | 65 | 80 | 30 | 800 | 4000 | 35 | 10 |

Table C. 2 -Basic stress-condition testing for use with the Arrhenius Method

| Test cell <br> number | Test stress <br> condition <br> (incubation) |  | Number of <br> specimens | Maximum <br> incubation <br> sub-interval <br> time | Minimum <br> total <br> incubation <br> time | Intermediate <br> RH | Minimum <br> equilibration <br> duration time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temp ( $\left.{ }^{\circ} \mathrm{C}\right)$ | $\% \mathrm{RH}$ |  | hours | hours | $\% \mathrm{RH}$ | hours |
| A | 85 | 80 | 20 | 250 | 1000 | 30 | 5 |
| B | 75 | 80 | 20 | 425 | 1700 | 33 | 7 |
| C | 65 | 80 | 30 | 600 | 2400 | 35 | 10 |

Regarding data analysis steps in Annex A and B, step 4 is replaced as follows.

Regression coefficients and the standard error can be calculated using the least squares method across all log time to failure data, which were obtained at the four or three stress conditions. This calculation can be performed by regression analysis of statistics software tools.

## C. 2 Data Analysis

## Step 1 and Step 2

For each stress condition, the specimens are ordered by increasing time to failure values. The median rank of the specimens is calculated using the estimate $(i-0,3) /(n+0,4)$. Table C .3 shows the result of ordered time to failure and median rank for three stress groups of $\mathrm{A}\left(85^{\circ} \mathrm{C}\right), \mathrm{B}\left(80^{\circ} \mathrm{C}\right), \mathrm{C}\left(75^{\circ} \mathrm{C}\right)$ and $\mathrm{D}\left(65^{\circ} \mathrm{C}\right)$, where relative humidity (RH) is kept constant $80 \%$.

Table C. 3 - Ordered time to failure and median rank for example data (Rigorous testing)

| Sample <br> Number | Sample Group and Stress Conditions ( 80 \%RH) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Group A (85 ${ }^{\circ} \mathrm{C}$ ) |  | Group B ( $80{ }^{\circ} \mathrm{C}$ ) |  | Group C ( $75{ }^{\circ} \mathrm{C}$ ) |  | Group D ( $65{ }^{\circ} \mathrm{C}$ ) |  |
|  | Time to Failure(h) | Median <br> Rank | Time to Failure(h) | Median Rank | Time to Failure(h) | Median Rank | Time to Failure(h) | Median Rank |
| 1 | 429 | 0,034 | 1015 | 0,034 | 1728 | 0,034 | 5455 | 0,023 |
| 2 | 451 | 0,083 | 1040 | 0,083 | 1882 | 0,083 | 5730 | 0,056 |
| 3 | 476 | 0,132 | 1080 | 0,132 | 1907 | 0,132 | 5908 | 0,089 |
| 4 | 484 | 0,181 | 1203 | 0,181 | 1989 | 0,181 | 6114 | 0,122 |
| 5 | 493 | 0,23 | 1151 | 0,23 | 2020 | 0,23 | 6326 | 0,155 |
| 6 | 495 | 0,279 | 1165 | 0,279 | 2076 | 0,279 | 6431 | 0,188 |
| 7 | 501 | 0,328 | 1193 | 0,328 | 2129 | 0,328 | 6544 | 0,22 |
| 8 | 512 | 0,377 | 1215 | 0,377 | 2151 | 0,377 | 6632 | 0,253 |
| 9 | 521 | 0,426 | 1230 | 0,426 | 2180 | 0,426 | 6711 | 0,286 |
| 10 | 526 | 0,475 | 1239 | 0,475 | 2227 | 0,475 | 6779 | 0,319 |
| 11 | 534 | 0,525 | 1260 | 0,525 | 2277 | 0,525 | 6860 | 0,352 |
| 12 | 540 | 0,574 | 1295 | 0,574 | 2318 | 0,574 | 6935 | 0,385 |
| 13 | 542 | 0,623 | 1310 | 0,623 | 2352 | 0,623 | 7038 | 0,418 |
| 14 | 548 | 0,672 | 1425 | 0,672 | 2404 | 0,672 | 7108 | 0,451 |
| 15 | 557 | 0,721 | 1360 | 0,721 | 2443 | 0,721 | 7202 | 0,484 |
| 16 | 576 | 0,77 | 1388 | 0,77 | 2512 | 0,77 | 7285 | 0,516 |
| 17 | 579 | 0,819 | 1420 | 0,819 | 2589 | 0,819 | 7362 | 0,549 |
| 18 | 586 | 0,868 | 1472 | 0,868 | 2590 | 0,868 | 7454 | 0,582 |
| 19 | 618 | 0,917 | 1540 | 0,917 | 2776 | 0,917 | 7562 | 0,615 |
| 20 | 645 | 0,966 | 1625 | 0,966 | 2891 | 0,966 | 7569 | 0,648 |
| 21 |  |  |  |  |  |  | 7710 | 0,681 |
| 22 |  |  |  |  |  |  | 7827 | 0,714 |
| 23 |  |  |  |  |  |  | 7955 | 0,747 |
| 24 |  |  |  |  |  |  | 8067 | 0,78 |
| 25 |  |  |  |  |  |  | 8250 | 0,813 |
| 26 |  |  |  |  |  |  | 8405 | 0,845 |
| 27 |  |  |  |  |  |  | 8546 | 0,878 |
| 28 |  |  |  |  |  |  | 8700 | 0,911 |
| 29 |  |  |  |  |  |  | 8953 | 0,944 |
| 30 |  |  |  |  |  |  | 9452 | 0,977 |

## Step 3

Figure C. 1 shows lognormal plot of groups A, B and C in Table C.1. Each best-fit straight line is drawn through the plotted data. If the lines are judged to be sufficiently parallel, the assumption of equivalent log standard deviation among the individual data sets is verified.


Figure C. 1 - Best fit lines of group A, B, C and D on lognormal paper (Verify that the fitting lines for all stress conditions are reasonably parallel to one another)

## Step 4

Table C. 4 shows total 90 sample data belong to specimen group $A, B, C$ and $D$ for regression analysis. Regression coefficients and error variance are calculated by applying the least squares method to 90 failure data sets which were obtained under the four stress conditions.

Table C. 5 shows the result of regression analysis by the statistics software tool. Residual error estimate $\hat{S} e$, standard error estimate $\hat{\sigma}$, and regression coefficient estimates $\hat{\beta}_{0}$ and $\hat{\beta}_{1}$ are obtained.

Table C. $4-90$ sample data for regression analysis


Table C. 5 - Results of regression Analysis

| Regression coefficients |  | Sum of squared <br> residual errors | Standard deviation <br> of residual errors |
| :---: | :---: | :---: | :---: |
| $\hat{\beta}_{0}$ | $\hat{\beta}_{1}$ | $\hat{S}_{e}$ | $\hat{\sigma}$ |
| $-36,2289$ | 15271,92 | 2,32868 | 0,16267 |

## Step 5

Using regression coefficient estimates $\hat{\beta}_{0}$ and $\hat{\beta}_{1}$ and standard error estimate $\hat{\sigma}$ in Table C.5, $\ln \hat{B}_{5}$ and $\ln \hat{B}_{50}$ can be calculated (see A.1.2).

Then $B_{5}$ Life, $B_{50}$ Life and the $95 \%$ lower confidence bound of $B_{5}$ Life at the Harsh storage condition $\left(30^{\circ} \mathrm{C}\right.$ and $80 \% \mathrm{RH}$ ) using calculated values of $\ln \hat{B}_{5}$ and $\ln \hat{B}_{50}$ are obtained as follows (see A.1.3).

$$
\begin{aligned}
& \begin{aligned}
\ln \hat{B}_{50}= & \hat{\beta}_{0}+\hat{\beta}_{1} x_{10} \\
& =-36,2289+15271,92 \times 0,0032987 \\
& =14,14856
\end{aligned} \\
& \begin{aligned}
& B_{50} \text { Life }=\exp (14,14856)=1395217 \text { hours (159 years) } \\
& \begin{aligned}
\ln \hat{B}_{5} & = \\
& \hat{\beta}_{0}+\hat{\beta}_{1} x_{10}-1,64 \hat{\sigma} \\
& =14,14856-1,64 \times 0,16267 \\
& =13,88178
\end{aligned} \\
& B_{5} \text { Life }=\exp (13,88178)=1068512 \text { hours (122 years) }
\end{aligned}
\end{aligned}
$$

$95 \%$ lower confidence bound of $B_{5}$ Life: $\left(B_{5} \text { Life }\right)_{\llcorner }$

$$
\begin{aligned}
& =\left(\exp \left(\ln \hat{B}_{5}\right)\right)_{L}=\exp \left(\ln \hat{B}_{5}+z_{5 / 100} \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right]}\right) \cong \exp \left(\ln \hat{B}_{5}-1.64 \hat{\sigma}\right) \\
& =\exp (13,88178-1,64 \times 0,16267)=\exp (13,6615) \\
& =818309 \text { hours (93 years) }
\end{aligned}
$$

## Annex D

(informative)

## Interval Estimation for $\boldsymbol{B}_{5}$ Life using Maximum Likelihood

## D. 1 Lower confidence bound

Lifetime estimation analysis (point estimation and simple interval estimation) for $B_{5}$ Life and $B_{50}$ Life are described in Annex A. In this annex, a more precise analysis method for interval estimation is introduced. One may consider only the lower bound of the confidence interval to estimate lifetime.

## D. 2 Maximum likelihood method

In order to $\log$ lifetime $y(=\ln t)$ is followed the normal distribution described in A.1.2, the likelihood function of parameters $\beta$ and $\sigma$ can be defined by the following equation.

$$
\begin{aligned}
L(\boldsymbol{\beta}, \sigma) & =\prod_{i=1}^{k} \prod_{j=1}^{n_{i}} f\left(y_{i j} \mid \boldsymbol{x}_{i}\right) \\
& =\prod_{i=1}^{k} \prod_{j=1}^{n_{i}} \frac{1}{\sqrt{2 \pi} \sigma} \exp \left\{-\frac{1}{2}\left(\frac{y_{i j}-\boldsymbol{x}^{\prime} \cdot \boldsymbol{\beta}}{\sigma}\right)^{2}\right\}
\end{aligned}
$$

where, $k$ denotes the number of specimen groups, $n_{i}$ denotes the number of specimens in the specimen group $j$.

The log likelihood function is then

$$
\ln L(\boldsymbol{\beta}, \sigma)=-\ln \sqrt{2 \pi} \sigma \sum_{i=1}^{k} n_{i}-\sum_{i=1}^{k} \sum_{j=1}^{n_{i}} y_{i j}-\frac{1}{2 \sigma^{2}} \sum_{i=1}^{k} \sum_{j=1}^{n_{i}}\left(y_{i j}-\left(\beta_{0}+\beta_{1} x_{1 i}+\beta_{2} x_{2 i}\right)\right)^{2}
$$

The maximum likelihood estimators of $\beta$ and $\sigma$ can be obtained by maximizing the third member of the equation.

The estimates $\hat{\beta}_{0}, \hat{\beta}_{1}$ and $\hat{\beta}$ are coefficients in the multiple regression equation, and the estimate $\hat{\sigma}$ is the standard deviation.

The point estimation of $\ln \hat{B}_{p}$ can be obtained using the estimates $\hat{\beta}_{0}, \hat{\beta}_{1}, \hat{\beta}_{2}$ and $\hat{\sigma}$ as

$$
\ln \hat{B}_{p}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{1}+\hat{\beta}_{2} x_{2}+z_{p / 100} \hat{\sigma} .
$$

Then the point estimates of 5 percentile and 50 percentile of the lifetime distribution are

$$
\begin{aligned}
& \ln \hat{B}_{5}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}-1,64 \hat{\sigma}, \text { and } \\
& \ln \hat{B}_{50}=\hat{\beta}_{0}+\hat{\beta}_{1} x_{10}+\hat{\beta}_{2} x_{20}
\end{aligned}
$$

## ecma

where $\left\{x_{10}, x_{20}\right\}$ denotes the Controlled storage condition ( $25^{\circ} \mathrm{C}$ and $50 \% \mathrm{RH}$ ).

Interval estimation for $\ln \hat{B}_{p}$ of optical disk, one may consider only lower bound. Therefore, $(100-\alpha) \%$ lower confidence bound of log lifetime $\ln \hat{B}_{p}$ is given as

$$
\left.\left(\ln \hat{B}_{p}\right)_{L}=\ln \hat{B}_{p}+z_{\alpha / 100} \sqrt{\operatorname{Var}\left[\ln \hat{B}_{p}\right]}\right) .
$$

As the variances of $\ln \hat{B}_{5}$ and $\ln \hat{B}_{50}$ are represented by $\operatorname{Var}\left[\ln \hat{B}_{5}\right]$ and $\operatorname{Var}\left[\ln \hat{B}_{50}\right]$ respectively, the $95 \%$ lower confidence bounds of $\ln \hat{B}_{5}$ and $\ln \hat{B}_{50}$ are given as follows.

$$
\begin{aligned}
& \left(\ln \hat{B}_{5}\right)_{L}=\ln \hat{B}_{5}-1,64 \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right]} \\
& \left(\ln \hat{B}_{50}\right)_{L}=\ln \hat{B}_{50}-1,64 \sqrt{\operatorname{Var}\left[\ln \hat{B}_{50}\right]}
\end{aligned}
$$

Where, $\operatorname{Var}\left[\ln \hat{B}_{5}\right]$ and $\operatorname{Var}\left[\ln \hat{B}_{50}\right]$ can be calculated by the following equations.

$$
\operatorname{Var}\left[\ln \hat{B}_{5}\right]=\left[\begin{array}{llll}
1 & x_{10} & x_{20} & -1.64
\end{array}\right]\left[\begin{array}{rrr}
\operatorname{var}\left[\hat{\beta}_{0}\right] & \operatorname{Cov}\left[\hat{\beta}_{0}, \hat{\beta}_{1}\right] & \operatorname{Cov}\left[\hat{\beta}_{0}, \hat{\beta}_{2}\right] \\
\operatorname{var}\left[\hat{\beta}_{1}\right] & \operatorname{Cov}\left[\hat{\beta}_{0}, \hat{\sigma}\right] \\
& \operatorname{Cov}\left[\hat{\beta}_{1}, \hat{\beta}_{2}\right] & \operatorname{Cov}\left[\hat{\beta}_{1}, \hat{\sigma}\right] \\
& \operatorname{var}\left[\hat{\beta}_{2}\right] & \operatorname{Cov}\left[\hat{\beta_{2}}, \hat{\sigma}\right] \\
& \operatorname{var}[\hat{\sigma}]
\end{array}\right]\left[\begin{array}{c}
1 \\
x_{10} \\
x_{20} \\
-1.64
\end{array}\right]
$$

$$
\operatorname{Var}\left[\ln \hat{B}_{50}\right]=\left[\begin{array}{lll}
1 & x_{10} & x_{20}
\end{array}\right]\left[\begin{array}{rr}
\operatorname{Var}\left[\hat{\beta}_{0}\right] & \operatorname{Cov}\left[\hat{\beta}_{0}, \hat{\beta}_{1}\right] \operatorname{Cov}\left[\hat{\beta}_{0}, \hat{\beta}_{2}\right] \\
\operatorname{Var}\left[\hat{\beta}_{1}\right] & \operatorname{Cov}\left[\hat{\beta}_{1}, \hat{\beta}_{2}\right] \\
\operatorname{Var}\left[\hat{\beta}_{2}\right]
\end{array}\right]\left[\begin{array}{c}
1 \\
x_{10} \\
x_{20}
\end{array}\right]
$$

NOTE
$\operatorname{Conv}\left\lfloor\hat{\beta}_{a}, \hat{\beta}_{b}\right\rfloor$ denotes covariance between $\hat{\beta}_{a}$ and $\hat{\beta}_{b}$.

Then, 95 \% lower confidence bounds of $\mathrm{B}_{5}$ Life is obtained as follows.

$$
\left(B_{5} \text { Life }\right)_{\mathrm{L}}=\left(\exp \left(\ln \hat{B}_{5}\right)\right)_{L}=\exp \left(\ln \hat{B}_{5}-1,64 \sqrt{\operatorname{Var}\left[\ln \hat{B}_{5}\right]}\right)
$$

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